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⑲ Applicant: SUMITOMO ELECTRIC INDUSTRIES,  
LTD  
5-33, Kitahama 4-chome,  
Chuo-ku  
Osaka-shi, Osaka-fu 541 (JP)

⑳ Inventor: Yoshimura, Masashi, c/o Itami  
Works of Sumitomo  
Elec. Ind. Ltd,  
1-1, Koyakita 1-chome  
Itami-shi, Hyogo (JP)  
Inventor: Yamamoto, Takehisa, c/o Itami  
Works of Sumitomo  
Elec. Ind. Ltd,

1-1, Koyakita 1-chome  
Itami-shi, Hyogo (JP)  
Inventor: Yamagata, Shinichi, c/o Itami Works of  
Sumitomo

Elec. Ind. Ltd,  
1-1, Koyakita 1-chome  
Itami-shi, Hyogo (JP)

Inventor: Matsui, Jin-Joo, c/o Itami Works of  
Sumitomo

Elec. Ind. Ltd,  
1-1, Koyakita 1-chome  
Itami-shi, Hyogo (JP)  
Inventor: Yamakawa, Akira, c/o Itami Works of  
Sumitomo

Elec. Ind. Ltd,

1-1, Koyakita 1-chome

Itami-shi, Hyogo (JP)

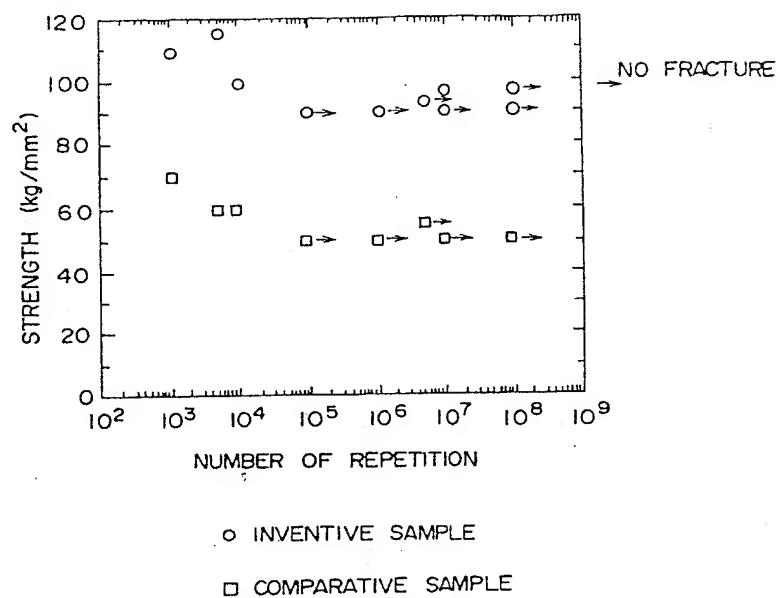
㉑ Representative: Fiener, Josef et al  
Patentanwälte Kahler, Käck & Fiener  
Postfach 12 49  
D-87712 Mindelheim (DE)

㉒ Silicon nitride sintered body.

㉓ Silicon nitride sintered bodies consisting of prismatic crystal grains of  $\text{Si}_3\text{N}_4$  and/or sialon, equi-axed crystal grains of  $\text{Si}_3\text{N}_4$  and/or sialon, a grain boundary phase existing among the prismatic and equi-axed crystal grains and dispersed particles in the grain boundary phase, in which the prismatic crystal grains have an average grain size of  $0.3 \mu\text{m}$  or less in minor axis and an average grain size of  $5 \mu\text{m}$  or less in major axis, the equi-axed crystal grains have an average grain size of  $0.5 \mu\text{m}$  or less and the dispersed particles have an average size of  $0.1 \mu\text{m}$  or less, the volume of the dispersed particles being  $0.05\%$  by volume or more based on the total volume of the rest of the sintered body. The silicon nitride sintered bodies have a strength sufficient for use as structural materials of machine parts or members, with a minimized scattering of the strength as well as high reliability, superior productivity and advantageous production cost.

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FIG. I



BACKGROUND OF THE INVENTION1. Field of the Invention

5 The present invention relates to silicon nitride sintered bodies which have superior mechanical properties at room temperature, with a minimized scattering of the properties, and also good productivity and cost efficiency.

2. Description of the Prior Art

10 Silicon nitride is a material well balanced in strength, fracture toughness, corrosion resistance, wear resistance, thermal shock resistance and oxidation resistance, etc., and has been extensively used in a wide variety of applications, such as cutting tools, frictionally sliding parts or other structural materials. However, there is the problem that this ceramic material is poor in strength and reliability as compared with metallic materials.

15 One reason for the poor strength of the silicon nitride sintered body is closely related to the grain boundary phase in the silicon nitride sintered body. The grain boundary phase is composed of a glass phase formed from a sintering aid, which is an indispensable component for sintering silicon nitride. In general, since this glass phase is brittle as compared with the matrix phase of the sintered body, it is highly susceptible to breakage when stress concentration is applied to the grain boundary phase. This causes the lowering of the strength of the sintered silicon nitride sintered body.

20 Therefore, various methods have hitherto been tried to improve the strength by reducing the grain boundary phase of a silicon nitride sintered body. For example, Japanese Patent Application Laid-Open (Kokai) Nos. 2-70715 and 3-117315 disclose techniques for reducing the thickness of a grain boundary phase by forming a grain-refined structure composed of equi-axed crystal grains of  $\alpha$ -Si<sub>3</sub>N<sub>4</sub> and prismatic crystal grains of  $\beta$ -Si<sub>3</sub>N<sub>4</sub>. However, in order to obtain fine  $\alpha$ -type crystal grains, a fine Si<sub>3</sub>N<sub>4</sub> powder having a high  $\alpha$ -ratio should be used as a starting material powder, resulting in a high production cost. Further, in order to ensure an improved strength properties in the resultant silicon nitride sintered body, the conversion rate to  $\beta$ -crystallization should be increased by sintering. However, in this sintering process, the  $\beta$ -type crystal grains grow to 2  $\mu$ m or more. Therefore, there is limitation in reducing the grain boundary phase only by the above-mentioned structural refinement technique.

25 Further, as disclosed in Japanese Patent Laid-Open Nos. 61-91065 and 2-44066, there has been known a method for combining equi-axed  $\alpha'$ -sialon having the general formula M<sub>x</sub>(Si,Al)<sub>12</sub>(O,N)<sub>16</sub> wherein M is at least one member selected from the group consisting of Mg, Ca, Li and rare earth elements and prismatic  $\beta'$ -sialon. This method improves the mechanical properties, such as strength, by the formation of a composite crystal phase. However, as is also apparent from the working examples disclosed in these applications, all the sintered bodies that stably have a bending strength exceeding 100 kg/mm<sup>2</sup> are obtained by a hot pressing process and this method is inappropriate to stably ensure high strength properties on an industrial scale.

30 40 As a further attempt for achieving an improved strength, fine foreign particles are dispersed in the structure of a silicon nitride sintered body to provide a composite structure. For example, Japanese Patent Laid Open No. 4-202059 discloses a method in which fine particles having a size of 1 to 500 nm are dispersed in prismatic silicon nitride or sialon having an average minor axis of 0.05 to 3  $\mu$ m and an aspect ratio of 3 to 20. However, although the working examples shows 167 kg/mm<sup>2</sup> as the highest strength, this method is highly liable to bring about the deterioration of the strength due to the presence of coarse silicon nitride and the Weibull coefficient is about 9 at the highest level. Therefore, there is a problem in stably obtaining high strength properties.

45 50 Japanese Patent Laid-Open No. 4-295056 discloses a method for dispersing particles of a foreign substance in the grain boundary phase of prismatic silicon nitride crystal grains. However, in this method, the prismatic silicon nitride crystal grains have a minor axis diameter and major axis diameter reaching, at the most, 2 to 3.5  $\mu$ m and 10 to 14  $\mu$ m, respectively. Therefore, the matrix per se acts as fracture origins and the strength shown in the working examples is only 158 kg/mm<sup>2</sup> at the highest. Further, since a high firing temperature of 1800°C or higher is required, the method is unsatisfactory also in productivity and cost.

SUMMARY OF THE INVENTION

In view of the problems encountered in the prior art, an object of the present invention is to provide silicon nitride sintered bodies which have a strength sufficient for use as structural materials of machine parts or members, with a minimized scattering of the strength as well as high reliability, superior productivity and advantageous production cost.

In order to achieve the above object, the present invention provides a silicon nitride sintered body consisting of prismatic crystal grains of  $\text{Si}_3\text{N}_4$  and/or sialon, equi-axed crystal grains of  $\text{Si}_3\text{N}_4$  and/or sialon, a grain boundary phase existing among these prismatic and equi-axed crystal grains and particles dispersed in the grain boundary phase, in which the prismatic crystal grains have an average grain size of 0.3  $\mu\text{m}$  or less in their minor axis and an average grain size of 5  $\mu\text{m}$  or less in their major axis and the equi-axed crystal grains have an average grain size of 0.5  $\mu\text{m}$  or less and the dispersed particles have an average particle size of 0.1  $\mu\text{m}$  or less, the volume of the dispersed particles being 0.05% by volume or more on the basis of the total volume of the rest of the sintered body.

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BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a graph showing a rotating bending fatigue limit;  
 FIG. 2 is an illustration showing the configuration of a test piece for a rotating bending fatigue test; and  
 20 FIG. 3 is a conceptual view of a rotary bending tester.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

In the present invention, in order to reduce the relative proportion of the grain boundary phase leading 25 to the deterioration of the strength of a silicon nitride sintered body, prismatic crystal grains and equi-axed crystal grains of silicon nitride and/or sialon are combined with a high filling density and, at the same, fine particles are dispersed within the grain boundary phase existing among the prismatic and equi-axed crystal gains. In such a microstructure, the surface area of the grain boundary phase is increased and the relative proportion of the glass phase is reduced. Further, it has been confirmed that, due to the existence of the 30 fine particles dispersed in the grain boundary phase, grain growth can be effectively prevented throughout the overall structure and a refined and uniform structure can be obtained by controlling the grain sizes of the prismatic crystal grains and the equi-axed crystal grains.

Consequently, in the silicon sintered body of the present invention, the prismatic and equi-axed crystal grains of silicon nitride and/or sialon are homogeneously refined and embrittlement in the grain boundary 35 phase can be reduced due to the reduced grain boundary phase. As a result, it is possible to stably ensure a strength of 160 kg/mm<sup>2</sup> or higher in terms of the three-point bending strength at room temperature according to JIS (Japanese Industrial Standards) R 1601 together with a high impact strength and an excellent fatigue property. The silicon nitride sintered body having such superior mechanical properties can be obtained at a low cost and in a good productivity. It has also been found that the silicon nitride sintered 40 body of the present invention are very suitable as a material for cutting tools because of its superior cutting properties.

In order to stably obtain the above-mentioned superior strength, it is required that the sintered body contains both of prismatic crystal gains ( $\beta$ -crystals) and equi-axed crystal grains ( $\alpha$ -crystals) wherein the prismatic crystal grains have an average grain size of not more than 0.3  $\mu\text{m}$  in minor axis and not more 45 than 5  $\mu\text{m}$  in major axis and the equi-axed crystal grains have an average grain size of not more than 0.5  $\mu\text{m}$ . When the average grain sizes of these crystal grains exceed the respective upper limits, the structure of the sintered body becomes nonuniform and coarse crystal grains act as fracture origins. Further, since the filling density of the prismatic crystal grains and equi-axed crystal grains is reduced and the thickness of the grain boundary phase is increased, strength reduction occurs in the resultant sintered body.

50 In the present invention,  $\alpha'$ -sialon and  $\beta'$ -sialon are solid solution crystal phases, respectively, represented by the general formula of  $\text{M}_x(\text{Si}, \text{Al})_{12}(\text{O}, \text{N})_{16}$  (wherein M is at least one member selected from the group consisting of Ti, Ni, Hf, V, Cr, Mg and rare earth elements and  $0 < x \leq 2.0$ ) and the general formula of  $\text{Si}_{6-z}\text{Al}_z\text{O}_z\text{N}_{8-z}$  (wherein  $0 < z \leq 4.2$ ).

The fine particles dispersed in the grain boundary phase have an average particle size of 0.1  $\mu\text{m}$  or less and the volume fraction occupied by the dispersed particles in the grain boundary phase should be at 55 least 0.05% by volume on the basis of the total volume of the remaining phases of the sintered body, excluding the dispersed particle phase. When the average particle size of the dispersed particles is greater than 0.1  $\mu\text{m}$ , besides particles exiting in the boundary grain phase, the quantity of particles existing in the

state of triple point or having the same size as the size of the equi-axed crystal grain size increases. Therefore, the relative quantity of the glass phase in the grain phase cannot be reduced and the overall grain growth becomes significant throughout the structure. As a result, desired strength levels cannot be achieved. By controlling the size of the dispersed particles to the above-specified particle size, the dispersed particles exhibit their effect of suppressing the grain growth in the whole structure, thereby providing a uniformly refined structure.

Further, when the volume of the dispersed particles in the grain boundary phase is less than 0.05% by volume based on the total volume of the rest of the sintered structure, the intended properties cannot be obtained since the reduction in the quantity of the glass phase is very small. On the other hand, when the volume of the dispersed particles is excessively large, the average particle size of the dispersed particles unavoidably becomes large. Therefore, it is necessary to control the volume of the dispersed particles in the grain boundary phase so that the average particle size of the particles does not exceed 0.1  $\mu\text{m}$ , preferably 0.03  $\mu\text{m}$  or less.

The dispersed particles are compounds other than silicon nitride and sialon. For example, compounds of Ti, Zr, Hf, V, Cr, etc., are used and among them Ti compounds are especially favorable. These compounds were confirmed to be present at least as nitride such as TiN, etc., in the sintered body by X-ray diffraction measurements.

Especially, when the dispersed particles are made of a titanium compound, the volume occupied by of the compound in the grain boundary phase is in the range of 0.05 to 4% by volume, preferably in the range of 0.05 to 2% by volume, on the basis of the total volume of the rest of the sintered body. When the volume percentage of the titanium compound is less than 0.05% by volume, the desired strength level cannot be obtained. On the other hand, when the volume percentage exceeds 4% by volume, the average particle size becomes greater due to the agglomeration of the titanium compound particles and defects are formed. Therefore, the required strength level cannot be achieved. Further, when the volume of the titanium compound exceeds 4% by volume, the sinterability of the powder raw material is lowered due to the presence of such an excessive titanium compound and a nonuniform part is formed in the resultant sintered body, thereby resulting in a reduction in the strength.

In order to obtain the silicon nitride sintered body of the present invention, a sintering aid capable of forming a liquid phase through the reaction with  $\text{SiO}_2$  present on the surface of the source powder of silicon nitride at a lowest possible temperature is used and such a sintering aid is exemplified by  $\text{Y}_2\text{O}_3$ ,  $\text{Al}_2\text{O}_3$ ,  $\text{MgO}$ ,  $\text{CeO}_2$ ,  $\text{CaO}$ , spinel or the like. A starting material powder mixture is molded into a green compact and subjected to sintering at a temperature not exceeding 1650 °C in a nitrogen gas atmosphere or other non-oxidizing atmosphere. Further, the sintered body is preferably subjected to secondary sintering in a pressurized non-oxidising atmosphere for further densification of the sintered body. The secondary sintering may be performed immediately after the first sintering or after cooling the first sintered body to room temperature.

In the present invention, as the starting material for the dispersed compound particles, exemplified by nitrides such as TiN, etc., compound powders, such as  $\text{TiO}_2$  powder or other oxide powder, capable of forming the dispersed compound particles during the sintering step are preferably used, although TiN powder or other nitride powder per se can also be used as the starting material. Especially when  $\text{TiO}_2$  powder is used as the starting material, its primary particle size is preferably 0.2  $\mu\text{m}$  or less to form dispersed particles containing TiN having an average particle size of 0.1  $\mu\text{m}$  or less.

In the present invention, since the dispersed particles, such as Ti compounds, etc., effectively prevent the grain growth during the sintering process, the aforesaid uniform fine structure comprising the  $\beta$ -type prismatic crystal grains and  $\alpha$ -type equi-axed crystal grains of silicon nitride and/or sialon can be obtained without requiring the use of an expensive fine silicon nitride source material powder having a high percentage  $\alpha$  crystallization. Since a low sintering temperature of 1650 °C or less can be employed, a continuous sintering furnace of pusher type or belt type or the like which is suitable for the mass production can be used. Therefore, it is unnecessary to conduct sintering in a pressurized atmosphere in order to suppress the sublimation of silicon nitride. Further, a highly densified sintered body having high strength can be easily obtained without sintering through a hot isostatic pressing (HIP). Therefore, the sintered body of the present invention is also advantageous in respect of productivity and cost.

Now, the present invention will be more specifically described with reference to the following examples.

55 Example 1

A commercially available  $\text{Si}_3\text{N}_4$  powder having an average grain size of 0.7  $\mu\text{m}$  and a percentage  $\alpha$  crystallization of 85% was mixed with sintering aid powders consisting of  $\text{Y}_2\text{O}_3$  powder,  $\text{Al}_2\text{O}_3$  powder and

MgO powder in the mixing ratios shown in Table 1. To each of the resultant mixtures, TiO<sub>2</sub> powder having a primary particle size of 30 nm was added as a source material for dispersed particles, in the amount shown in Table 1. The added amount of TiO<sub>2</sub> is shown by weight percentage (wt.%) based on the total weight of the other starting powder materials, excluding TiO<sub>2</sub>. Hereinafter, the amounts of TiO<sub>2</sub> or other source materials to be dispersed as fine particles in the resultant sintered bodies are all represented by weight percent based on the total weight of other starting powder materials. The above powders were wet-mixed in ethanol for 100 hours in a nylon ball mill and subjected to CIP (Cold Isostatic Press) molding under a pressure of 3000 kg/cm<sup>2</sup>.

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Table 1

	Sample	Si <sub>3</sub> N <sub>4</sub> (wt.%)	Y <sub>2</sub> O <sub>3</sub> (wt.%)	Al <sub>2</sub> O <sub>3</sub> (wt.%)	MgO (wt.%)	TiO <sub>2</sub> (wt.%)
15	1	91	5	3	1	0.1
	2	91	5	3	1	0.2
	3	91	5	3	1	1.0
	4	91	5	3	1	5.0
	5	91	5	3	1	8.0
20	6	93	4	2	1	0.6
	7	98	1	0.5	0.5	0.4
	8*	91	5	3	1	0
	9*	91	5	3	1	0.02
	10*	91	5	3	1	15.0
25	11*	91	5	3	1	20.0

\* Comparative Samples

Each green compact thus molded was subjected to primary sintering in a nitrogen gas atmosphere under a pressure of 1 atm at 1500 °C for 4 hours and, then, subjected to secondary sintering in a nitrogen gas atmosphere under a pressure of 1000 atm at 1600 °C for 1 hour. 15 bending test pieces each having a size of 3 mm x 4 mm x 40 mm were cut out of each sintered body and finished through grinding with a # 800 grinding diamond wheel. The three-point bending strength test was conducted for each test piece at room temperature according to JIS R 1601 and the average bending strength and Weibull coefficient were measured.

For each sintered body, the relative density was measured and the  $\alpha, \alpha' : \beta, \beta'$  ratio of two types of crystals was obtained from the ratio of the peak intensities of  $\alpha$ - (including  $\alpha'$ ) equi-axed crystals to  $\beta$ - (including  $\beta'$ ) prismatic crystals, namely  $(I_{\alpha} + I_{\alpha'}) : (I_{\beta} + I_{\beta'})$  wherein  $I_{\alpha}, I_{\alpha'}, I_{\beta}$  and  $I_{\beta'}$  are the respective peak intensities of  $\alpha$ - and  $\alpha'$ - equi-axed crystals and  $\beta$ - and  $\beta'$ - prismatic crystals, measured by X-ray diffraction.

In order to measure the average diameters of equi-axed grains of  $\alpha$ -Si<sub>3</sub>N<sub>4</sub> and/or  $\alpha'$ -sialon and prismatic grains of  $\beta$ -Si<sub>3</sub>N<sub>4</sub> and/or  $\beta'$ -sialon, each sintered body was subjected to lapping and etching treatments at its arbitrary surface and the thus treated surface was observed at 10 areas thereof under a scanning electron microscope (magnification: x 5,000). The average diameters of the equi-axed grains of  $\alpha$ -Si<sub>3</sub>N<sub>4</sub> and/or  $\alpha'$ -sialon were determined by measuring the average diameters of circular grains. The average diameter in minor axis of the prismatic grains of  $\beta$ -Si<sub>3</sub>N<sub>4</sub> and/or  $\beta'$ -sialon was determined from the average diameters in the direction of the minor axis of square-shaped or rectangular grains and the average diameter in major axis of the prismatic grains was determined from the average diameters in the direction of the major axis of rectangular grains. Further, the average particle sizes and volume proportions (vol.%) of Ti compounds present in the grain boundary phase were determined from observation of 10 areas with a transmission electron microscopy (magnification: x 40,000). The volume proportion of the Ti compounds present in the grain boundary phase to the rest of the sintered body was calculated by raising the area proportion of the Ti compounds in the grain boundary phase to the 3/2 power, i.e.,  $\sqrt{\text{area proportion of Ti compounds in grain boundary phase}}^3$ .

Table 2

Sample	Relative density	Ratio of $\alpha, \alpha'$ ; $\beta, \beta'$ crystal grain size (%)	Equi-axed crystal grain size (nm)		Prismatic crystal grain size (nm)		Dispersed Ti compounds	
			Minor axis (nm)	Major axis (nm)	Minor axis (nm)	Major axis (nm)	Particle size (nm)	Volume proportion (vol. %)
1	99.2	15:85	350	250	2.0	2.0	30	0.05
2	99.4	15:85	300	240	2.0	2.0	30	0.1
3	99.2	13:87	300	230	2.0	2.0	30	0.5
4	99.1	9:91	250	200	2.0	2.0	50	2.4
5	99.4	8:92	250	200	1.5	1.5	90	4.0
6	99.3	17:83	250	200	2.0	2.0	40	0.3
7	99.1	17:83	300	250	2.0	2.0	30	0.2
8*	99.0	16:84	400	330	2.5	2.5	-	0
9*	99.0	9:91	320	290	2.5	2.5	30	0.01
10*	97.2	9:91	300	300	1.5	1.5	350	7.0
11*	96.9	5:95	300	330	1.0	1.0	400	10.0

\* Comparative Samples

Table 3

	Sample	Bending strength (kg/mm <sup>2</sup> )	Weibull coefficient
5	1	175	24
	2	190	25
	3	213	29
	4	180	24
	5	170	23
10	6	172	22
	7	176	26
	8*	130	17
	9*	115	15
	10*	111	10.2
15	11*	100	9.5

\* Comparative Samples

It is clear from the above results that the samples of the present invention all have a high bending strength of at least 170 kg/mm<sup>2</sup> and, as shown from a Weibull coefficient of at least 22, scattering in their strength values is small. In contrast to this, it is clear that comparative samples 8 and 9 are not improved in their strength because of insufficient volume percentage of the dispersed particles and comparative samples 10 and 11 are subjected to strength reduction because of excessively high volume percentages of the dispersed particles and too large particle sizes of the same.

25 Example 2

The same starting material powders as those used in Example 1 were mixed in the respective mixing ratios shown in Table 4. Sample Nos. 2 and 8 had the same compositions as those in Example 1. The 30 resultant mixtures were molded in the same manner as described in Example 1 and were subjected to primary sintering and secondary sintering in a nitrogen gas atmosphere under the conditions shown in Table 5.

Table 4

	Sample	Si <sub>3</sub> N <sub>4</sub> (wt.%)	Y <sub>2</sub> O <sub>3</sub> (wt.%)	Al <sub>2</sub> O <sub>3</sub> (wt.%)	MgO (wt.%)	TiO <sub>2</sub> (wt.%)
40	2	91	5	3	1	0.2
	12	91	5	3	1	0.8
	13	89	6	4	1	2.1
	14	85	10	4	1	6.3
	8*	91	5	3	1	0
	15*	89	6	4	1	10.5

45 \* Comparative Samples

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Table 5

5	Sample	Primary sintering conditions		Secondary sintering conditions	
		Temp.(°C)	Pressure (atm)	Temp.(°C)	Pressure (atm)
10	2-A	1525	1	1600	500
	2-B	1550	10	1650	10
	2-C	1475	1	1700	5
	2-D	1475	1	1600	1000
	2-E	1600	1	1600	50
	12-F	1475	1	1575	1000
	13-G	1500	2	1600	100
	14-H	1450	1	1650	30
	14-I	1575	1	1750	5
	8-J*	1550	1	1650	10
15	8-K*	1500	1	1700	5
	15-L*	1600	1	1600	50
	15-M*	1475	1	1600	1000

20 \* Comparative Samples

25 Each sample of the thus obtained sintered bodies was measured for relative density,  $\alpha$ ,  $\alpha'$  :  $\beta$ ,  $\beta'$  ratio, average grain sizes in the major axis and minor axis of prismatic crystal grains of  $\beta$ - $\text{Si}_3\text{N}_4$  and/or  $\beta'$ -sialon, average grain size of equi-axed crystal grains of  $\alpha$ - $\text{Si}_3\text{N}_4$  and/or  $\alpha'$ -sialon, average particle size of the dispersed particles and volume percentage (vol. %) of the dispersed particles in the grain boundary phase on the basis of the total volume of the rest (excluding the dispersed particles) of the sintered body, in the same manner as described in Example 1. Further, the three-point bending strength and Weibull coefficient were measured for each sample at room temperature in the same procedures as set forth in Example 1. The results are given in Tables 6 and 7.

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Table 6

Sample	Relative density	Ratio of $\alpha, \alpha'$ : $\beta, \beta'$	Equi-axed crystal grain size (nm)	Prismatic crystal grain size		Dispersed Ti compounds	
				Minor axis	Major axis	Particle size (nm)	Volume proportion (vol. %)
2-A	99.2	16:84	300	230	2.0	30	0.1
2-B	99.0	4:96	300	250	1.7	30	0.1
2-C	98.8	19:81	350	200	2.5	30	0.1
2-D	99.3	10:90	250	200	2.0	30	0.1
2-E	99.2	10:90	300	200	2.0	30	0.1
12-F	99.5	17:83	200	200	2.5	30	0.4
13-G	99.0	16:84	300	250	2.0	60	1.0
14-H	98.5	10:90	350	200	1.8	100	3.0
14-I	98.9	16:84	350	200	2.3	60	3.0
8-J*	97.5	25:75	500	300	1.5	-	0
8-K*	98.5	16:84	300	300	1.6	-	0
15-L*	96.2	7:93	450	200	1.0	200	5.0
15-M*	98.3	1:99	450	350	1.0	200	5.0

\* Comparative Samples

Table 7

Sample	Bending strength (kg/mm <sup>2</sup> )	Weibull coefficient
2-A	180	23
2-B	181	21
2-C	160	20
2-D	200	25
2-E	175	24
12-F	213	27
13-G	165	25
14-H	162	24
14-I	160	22
8-J*	120	9
8-K*	116	11
15-L*	115	11
15-M*	120	7

\* Comparative Samples

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Example 3

Compositions as shown in Table 8 were prepared using the same starting materials as used in Example 25 1 except that the primary particle size of the TiO<sub>2</sub> powder was varied as shown in Table 8. Similarly to Example 1, each powder mixture was molded into a green compact and subjected to primary sintering in a 1-atm nitrogen gas atmosphere at 1500 °C for 4 hours and, then, secondary sintering in a 1000-atm nitrogen gas atmosphere at 1600 °C for one hour.

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Table 8

Sample	Si <sub>3</sub> N <sub>4</sub> (wt.%)	Y <sub>2</sub> O <sub>3</sub> (wt.%)	Al <sub>2</sub> O <sub>3</sub> (wt.%)	MgO (wt.%)	TiO <sub>2</sub> (wt.%)	TiO <sub>2</sub> (nm **)
16-1	91	5	3	1	0.4	15
16-2	91	5	3	1	0.4	30
16-3*	91	5	3	1	0.4	300
17-1	89	5	4	2	0.4	15
17-2	89	5	4	2	0.4	50
17-3*	89	5	4	2	0.4	200
18-1	89	6	4	1	2.1	100
18-2*	89	6	4	1	2.1	500

\* Comparative Samples

\*\* Primary particle size

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Each sample of the thus obtained sintered bodies was measured for relative density,  $\alpha$ ,  $\alpha' : \beta$ ,  $\beta'$  ratio, average grain sizes in the major axis and minor axis of prismatic crystal grains of  $\beta$ -Si<sub>3</sub>N<sub>4</sub> and/or  $\beta'$ -sialon, average grain size of equi-axed crystal grains of  $\alpha$ -Si<sub>3</sub>N<sub>4</sub> and/or  $\alpha'$ -sialon, average particle size of the dispersed particles and volume percentage (vol. %) of the dispersed particles in the grain boundary phase on the basis of the total volume of the rest (excluding the dispersed particles) of the sintered body, in the same manner as described in Example 1. Further, the three-point bending strength and Weibull coefficient were measured for each sample at room temperature in the same procedures as set forth in Example 1. The results are given in Tables 9 and 10.

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Table 9

Sample	Relative density	Ratio of $\alpha, \alpha'$ : $\beta, \beta'$ crystal grain size (%)	Equi-axed grain size (nm)	Prismatic crystal grain size (nm)	Dispersed Ti compounds		
					Minor axis	Major axis	Volume proportion (vol. %)
16-1	99.4	11:89	350	250	2.0	15	0.2
16-2	99.3	16:84	300	200	2.0	20	0.2
16-3*	97.5	21:79	300	250	1.5	300	0.2
17-1	99.5	14:86	250	200	2.0	15	0.3
17-2	99.1	15:85	250	200	1.8	50	0.3
17-3*	96.2	16:84	320	250	1.5	250	0.3
18-1	99.3	14:86	330	250	2.0	100	1.0
18-2*	98.2	16:84	400	350	1.5	500	1.0

\* Comparative Samples

Table 10

Sample	Bending strength (kg/mm <sup>2</sup> )	Weibull coefficient
16-1	192	22
16-2	171	20
16-3*	123	8
17-1	189	23.6
17-2	196	25.3
17-3*	143	12
18-1	161	21
18-2*	139	16.2

\* Comparative Samples

15 The above results reveal that when  $TiO_2$  powder having a large primary particle size is used as a source material powder for Ti compounds dispersed particles, the particle dispersed in the resultant sintered body also have a large particle size. When the average particle size of the dispersed particles exceeds 0.1  $\mu m$ , the bending strength and Weibull coefficient decrease and scattering in the properties 20 becomes significant.

Example 4

25 Compositions as shown in Table 11 were prepared using the same starting materials as used in Example 1 except that the primary particles size of the  $TiO_2$  powder was varied as shown in Table 11. Samples 4, 8 and 11 had the same compositions as those used in Example 1. Similarly to Example 1, each powder mixture was molded into a green compact and subjected to primary sintering in a 1-atm nitrogen gas atmosphere at 1500 °C for 4 hours and, then, secondary sintering in a 1000-atm nitrogen gas atmosphere at 1575 °C for one hour.

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Table 11

Sample	Si <sub>3</sub> N <sub>4</sub> (wt.%)	Y <sub>2</sub> O <sub>3</sub> (wt.%)	Al <sub>2</sub> O <sub>3</sub> (wt.%)	MgO (wt.%)	TiO <sub>2</sub> (wt.%)	TiO <sub>2</sub> (nm **)
4	91	5	3	1	5.0	15
19	91	5	3	1	0.4	100
8*	91	5	3	1	0	-
11*	91	5	3	1	20.0	30

\* Comparative Samples

\*\* Primary particle size

45 Test chips were cut from the respective sintered body and subjected to a cutting test under the conditions shown in Table 12. The respective test results are shown in Table 13. The criterion of the judgment on the life of the chips was made by measuring the cutting time providing a flank wear width of 0.3 mm.

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Table 12

		Cutting test 1	Cutting test 2
5	Cutting work	Lathing (wet-type)	Milling (wet-type)
	Material to be machined	FC25(H <sub>B</sub> 180)	FC25(H <sub>B</sub> 200)
	Cutting speed	800m/min	400m/min
10	Feed	1mm/rev.	0.5mm/tip
	Depth of cut	2mm	4mm

Table 13

Sample	Life of Chips (min)	
	Cutting Test 1	Cutting Test 2
20	4	35
	19	40
	8*	5
	11*	3
25		55
		50
		10
		7

\* Comparative samples

It can be seen from the above results that the silicon nitride sintered bodies of the present invention exhibit superior cutting performance both in continuous cutting and intermittent cutting and is suitable as cutting tools.

#### Example 5

The respective oxide powders as shown in Table 14 were used as source powders for dispersed particles. Each oxide powder was mixed with the other starting material powders, which were the same as those used in Example 1, in the mixing ratios specified in Table 14. Each of the resulting powder mixtures was molded into a green compact and subjected to primary sintering in a 1-atm nitrogen gas atmosphere at 1500 °C for 4 hours and, then, secondary sintering in a 1000-atm nitrogen gas atmosphere at 1600 °C for one hour.

Table 14

Sample	Si <sub>3</sub> N <sub>4</sub> (wt.%)	Y <sub>2</sub> O <sub>3</sub> (wt.%)	Al <sub>2</sub> O <sub>3</sub> (wt.%)	MgO (wt.%)	Added oxide (wt.%)
45	20	91	5	3	1
	21	91	5	3	1
	22	91	5	3	1
	23	91	5	3	1
					ZrO <sub>2</sub> 1.8
					HfO <sub>2</sub> 1.0
					V <sub>2</sub> O <sub>3</sub> 1.0
					Cr <sub>2</sub> O <sub>3</sub> 1.0

50 Each sample of the thus obtained sintered bodies was measured for relative density,  $\alpha$ ,  $\alpha'$ :  $\beta$ ,  $\beta'$  ratio, average grain sizes in the major axis and minor axis of prismatic crystal grains of  $\beta$ -Si<sub>3</sub>N<sub>4</sub> and/or  $\beta'$ -sialon, average grain size of equi-axed crystal grains of  $\alpha$ -Si<sub>3</sub>N<sub>4</sub> and/or  $\alpha'$ -sialon, average particle size of the dispersed particles and volume percentage (vol. %) of the dispersed particles in the grain boundary phase on the basis of the total volume of the rest (excluding the dispersed particles) of the sintered body, in the same manner as described in Example 1. Further, the three-point bending strength and Weibull coefficient were measured for each sample at room temperature in the same procedures as set forth in Example 1. The results are given in Tables 15 and 16.

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Table 15

Sample	Relative density	Ratio of $\alpha, \alpha'$ : $\beta, \beta'$ crystal grain size (%)	Equi-axed crystal grain size (nm)		Prismatic crystal grain size (nm)		Dispersed compounds	
			Minor axis	Major axis	Minor axis	Major axis	Volume proportion (vol. %)	
20	99.5	7:93	300	250	2.0	5.0	0.2	
21	99.3	8:92	300	200	1.5	10.0	0.2	
22	99.4	10:90	300	250	1.8	10.0	0.2	
23	99.3	5:95	300	250	1.5	10.0	0.2	

\* Comparative Samples

Table 16

Sample	Bending strength (kg/mm <sup>2</sup> )	Weibull coefficient
20	170	23
21	165	20
22	167	20
23	165	23

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Example 6

15 A commercially available  $\text{Si}_3\text{N}_4$  powder having an average grain size of 0.7  $\mu\text{m}$  was mixed with compounds of Y, Al and Mg in the mixing ratios, by weights in terms of their oxides, shown in Table 17. To each mixture, titanium oxide powder having a primary particle size of 15 nm was added, as a source material for dispersed particles, in the amount shown in Table 17. The above powders were wet-mixed in ethanol for 100 hours in a nylon ball mill and subjected to CIP molding under a pressure of 3000 kg/cm<sup>2</sup>.

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Table 17

Samples	$\text{Si}_3\text{N}_4$ (wt.%)	$\text{Y Y}_2\text{O}_3$ (wt.%)	$\text{Al Al}_2\text{O}_3$ (wt.%)	$\text{Mg MgO}$ (wt.%)	$\text{TiO}_2$ (wt.%)
Samples of the present invention					
1	91	5	3	1	0.1
2	91	5	3	1	0.2
3	91	5	3	1	1.0
4	91	5	3	1	2.0
5	91	5	3	1	4.0
6	93	4	2	1	0.7
7	98	1	0.5	0.5	0.4
Comparative samples					
1	91	5	3	1	0
2	91	5	3	1	0.02
3	91	5	3	1	15.0
4	91	5	3	1	20.0

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Each of the green compacts shown in Table 17 was subjected to primary sintering in a nitrogen gas atmosphere under a pressure of 1 atm at 1500 °C for 4 hours and, then, subjected to secondary sintering in a nitrogen gas atmosphere under a pressure of 1000 atm at 1575 °C for 1 hour.

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Each sample of the thus obtained sintered bodies was measured for relative density,  $\alpha$ ,  $\alpha'$  :  $\beta$ ,  $\beta'$  ratio, average grain sizes in the major axis and minor axis of prismatic crystal grains of  $\beta\text{-Si}_3\text{N}_4$  and/or  $\beta'\text{-sialon}$ , average grain size of equi-axed crystal grains of  $\alpha\text{-Si}_3\text{N}_4$  and/or  $\alpha'\text{-sialon}$ , average particle size of the dispersed particles and volume percentage (vol. %) of the dispersed particles in the grain boundary phase on the basis of the total volume of the rest (excluding the dispersed particles) of the sintered body, in the same manner as described in Example 1. Further, the three-point bending strength and Weibull coefficient were measured for each sample at room temperature in the same procedures as set forth in Example 1. The results are shown in Table 18.

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Table 18

5	Samples	Relative density* (%)	$\alpha, \alpha' : \beta, \beta'$	3-Point bending strength	Weibull coefficient (kg/mm <sup>2</sup> )
<u>Samples of the present invention</u>					
15	1	99.3	17 : 83	185	24.5
	2	99.5	16 : 84	200	28
	3	99.2	14 : 86	235	29
20	4	99.1	11 : 89	190	26
	5	99.3	9 : 81	180	27
	6	99.4	16 : 84	204	26
	7	99.1	17 : 83	186	27
25	<u>Comparative samples</u>				
	1	99.0	19 : 81	135	18.5
30	2	99.0	9 : 91	121	18
	3	97.2	9 : 91	120	10.2
	4	97.0	5 : 95	105	9.5

35 \*Relative density of secondary sintered body

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Table 18 (continued)

Samples	Equi-axed crystal grain size (nm)	Prismatic crystal grain size			Dispersed Ti compounds		
		Minor axis (nm)	Major axis ( $\mu\text{m}$ )	size (nm)	Particle size (nm)	Volume proportion (vol. %)	
<u>Samples of the present invention</u>							
1	350	250	2.0	1.5	0.05		
2	300	240	2.0	1.5	0.1		
3	300	230	2.0	1.5	0.5		
4	250	200	2.0	2.0	1.0		
5	250	200	2.0	3.0	2.0		
6	320	250	2.0	3.0	0.3		
7	300	260	2.0	2.0	0.2		
<u>Comparative samples</u>							
1	400	330	2.5	-	0		
2	300	290	2.5	15	0.01		
3	300	300	1.5	200	7.0		
4	300	300	1.0	300	10.0		

Example 7

Green compacts having the compositions shown in Table 19 were prepared by using the same powders as used in Example 6 and subjected to primary sintering in a nitrogen gas and secondary sintering in a nitrogen gas, under the conditions specified in Table 20. The secondary sintering may be performed either immediately after the primary sintering or after cooling each primary sintered body to room temperature, under the specified secondary sintering conditions.

Each sample of the thus obtained sintered bodies was measured for relative density,  $\alpha$ ,  $\alpha'$  :  $\beta$ ,  $\beta'$  ratio, average grain sizes in the major axis and minor axis of prismatic crystal grains of  $\beta\text{-Si}_3\text{N}_4$  and/or  $\beta'\text{-sialon}$ , average grain size of equi-axed crystal grains of  $\alpha\text{-Si}_3\text{N}_4$  and/or  $\alpha'\text{-sialon}$ , average particle size of the dispersed particles and volume percentage (vol. %) of the dispersed particles in the grain boundary phase on the basis of the total volume of the rest (excluding the dispersed particles) of the sintered body, in the same manner as described in Example 1. Further, the three-point bending strength and Weibull coefficient

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were measured for each sample at room temperature in the same procedures as set forth in Example 1. The results are shown in Table 21.

Table 19

Sample	Si <sub>3</sub> N <sub>4</sub> (wt.%)	Y <sub>2</sub> O <sub>3</sub> (wt.%)	Al <sub>2</sub> O <sub>3</sub> (wt.%)	MgO (wt.%)	TiO <sub>2</sub> (wt.%)
Samples of the present invention					
2	91	5	3	1	0.2
8	91	5	3	1	0.8
9	89	6	4	1	2.1
10	85	10	4	1	3.2
Comparative samples					
1	91	5	3	1	-
5	89	6	4	1	10.5

Table 20

Sample	Primary sintering		Secondary sintering	
	Temp. (°C)	Pressure (atm)	Temp. (°C)	Pressure (atm)
Samples of the present invention				
2-A	1525	1	1600	500
2-B	1550	10	1650	10
2-C	1475	1	1700	5
2-D	1475	1	1600	1000
2-E	1600	1	1600	50
8-F	1475	1	1575	1000
9-G	1500	2	1600	100
10-H	1450	1	1650	30
10-I	1575	1	1750	5
Comparative samples				
1-J	1550	1	1650	10
1-K	1500	1	1700	5
5-L	1600	1	1600	50
5-M	1475	1	1600	1000

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Table 21

5	Sample	Relative density* (%)	$\alpha, \alpha' : \beta, \beta'$	3-Point bending strength (kg/mm <sup>2</sup> )	Weibull coefficient
<u>10</u>					
	<u>Samples of the present invention</u>				
15	2-A	99.3	17 : 83	193	24.2
	2-B	99.1	5 : 95	190	23
	2-C	98.9	19 : 81	170	22
20	2-D	99.5	11 : 89	213	26
	2-E	99.2	10 : 90	179	25
	8-F	99.6	15 : 85	225	28.3
	9-G	99.0	18 : 82	175	26
25	10-H	98.9	12 : 88	177	25.5
	10-I	99.2	19 : 81	170	24
<u>30</u>					
	<u>Comparative samples</u>				
35	1-J	97.5	25 : 75	120	9
	1-K	98.5	16 : 84	116	11
	5-L	96.2	9 : 91	125	13
	5-M	98.3	3 : 97	130	8

\* Relative density of secondary sintered body

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Table 21 (continued)

Samples	Equi-axed crystal grain size (nm)	Prismatic crystal grain size		Dispersed Ti compounds		
		Minor axis (nm)	Major axis ( $\mu$ m)	Particle size (nm)	Volume proportion (vol. %)	
<u>Samples of the present invention</u>						
2-A	350	250	2.0	15	0.1	
2-B	350	280	1.8	15	0.1	
2-C	400	300	2.4	15	0.1	
2-D	250	200	2.0	15	0.1	
2-E	300	250	2.0	15	0.1	
8-F	250	200	1.8	15	0.4	
9-G	300	260	2.0	20	1.0	
10-H	400	300	1.5	30	1.5	
10-I	420	300	2.5	50	1.5	
<u>Comparative samples</u>						
1-J	500	300	1.5	-	-	
1-K	300	300	1.6	-	-	
5-L	500	200	1.0	100	5.0	
5-M	500	400	1.0	100	5.0	

Example 8

Using three different kinds of compositions as shown in Table 22, sintered bodies were prepared by 50 performing primary sintering in a 1-atm nitrogen gas at 1500°C for 1 hr and secondary sintering in a 500-atm nitrogen gas at 1600°C for 4 hr. In the compositions, the primary particle size of titanium oxide was changed as shown in Table 22.

Each sample of the thus obtained sintered bodies was measured for relative density,  $\alpha$ ,  $\alpha' : \beta$ ,  $\beta'$  ratio, average grain sizes in the major axis and minor axis of prismatic crystal grains of  $\beta$ - $\text{Si}_3\text{N}_4$  and/or  $\beta'$ -sialon, average grain size of equi-axed crystal grains of  $\alpha$ - $\text{Si}_3\text{N}_4$  and/or  $\alpha'$ -sialon, average particle size of the dispersed particles and volume percentage (vol. %) of the dispersed particles in the grain boundary phase on the basis of the total volume of the rest (excluding the dispersed particles) of the sintered body, in the same manner as described in Example 1. Further, the three-point bending strength and Weibull coefficient

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were measured for each sample at room temperature in the same procedures as set forth in Example 1. The results are shown in Table 23.

Table 22

Sample	Si <sub>3</sub> N <sub>4</sub> (wt.%)	Y <sub>2</sub> O <sub>3</sub> (wt.%)	Al <sub>2</sub> O <sub>3</sub> (wt.%)	MgO (wt.%)	TiO <sub>2</sub>	
					(wt.%)	(nm) <sup>**</sup>
11-1	91	5	3	1	0.4	15
11-2	91	5	3	1	0.4	30
11-3*	91	5	3	1	0.4	100
12-1	89	5	4	2	0.4	15
12-2	89	5	4	2	0.4	50
12-3*	89	5	4	2	0.4	200
13-1	89	6	4	1	2.1	15
13-2*	89	6	4	1	2.1	150

\* Comparative samples

\*\* Primary particle size

Table 23

Sample	Relative density** $\alpha, \alpha' : \beta, \beta'$ (%)	3-Point bending strength	Weibull coefficient (kg/mm <sup>2</sup> )
11-1	99.4	11 : 89	192
11-2	99.3	16 : 84	171
11-3*	98.6	19 : 81	143
12-1	99.5	14 : 86	189
12-2	99.1	15 : 85	196
12-3*	96.2	16 : 84	143
13-1	99.5	16 : 84	201
13-2*	98.2	16 : 84	139

\* Comparative samples

\*\* Relative density of secondary sintered body

Table 23 (continued)

Samples	Equi-axed crystal	Prismatic crystal			Dispersed Ti compounds		
		grain size (nm)	Minor axis (nm)	Major axis (μm)	Particle size (nm)	Volume (μm)	Percentage (vol.-%)
11-1	350	250	2.0	1.5	15	0.2	
11-2	300	200	2.0	20	20	0.2	
11-3*	300	250	1.8	80	80	0.2	
12-1	250	200	2.0	1.5	1.5	0.3	
12-2	250	200	2.0	50	50	0.3	
12-3*	320	250	1.5	200	200	0.3	
13-1	300	260	2.0	30	30	1	
13-2*	400	350	1.0	500	500	1	

\* Comparative samples

#### Example 9

Starting materials having the compositions shown in Table 24 were subjected to sintering at 1500°C for 4 hr under atmospheric pressure and secondary sintering in a 1000-atm nitrogen gas atmosphere at 50 1575°C for 1 hr. Each of the thus obtained sintered bodies was subjected to the Charpy impact test and fatigue test.

According to JIS 1601, the Charpy test was conducted under conditions of a Charpy capacity of 1.5 kgfcm and an impact speed of 0.76 m/sec. The fatigue test was conducted in accordance with Ono's rotating bending testing method (diameter of the evaluated portion: 6 mm, diameter of the fixing portions at 55 both ends: 8 mm and gauge length: 12 mm). The dimensions of the tested specimen are shown in millimeter units in FIG. 2 and the conceptual view of the used tester is shown in FIG. 3. In FIG. 3, reference numerals are as follows.

1: specimen, 2: specimen fixing portion, 3: weight

The results of the Charpy impact test are shown in Table 25 and the results of the fatigue test are shown in FIG. 1.

Table 24

Sample	Si <sub>3</sub> N <sub>4</sub> (wt.%)	Y <sub>2</sub> O <sub>3</sub> (wt.%)	Al <sub>2</sub> O <sub>3</sub> (wt.%)	MgO (wt.%)	TiO <sub>2</sub> (wt.%)
Samples of the present invention					
1	91	5	3	1	0.10
8	91	5	3	1	0.8
Comparative samples					
1	91	5	3	1	0
4	91	5	3	1	20.0

Table 25

Samples	Charpy impact value (kgm/cm <sup>2</sup> )
Samples of the present invention	
1	0.20
8	0.24
Comparative samples	
1	0.15
4	0.11

It can be seen from the above results that the samples of the present invention have a high impact value and a good fatigue strength as compared with the comparative samples.

According to the present invention, there is provided silicon nitride sintered bodies which have superior mechanical properties, such as a three-point bending strength of at least 160 kg/mm<sup>2</sup> at room temperature, with a minimized scattering in the strength properties, and also high reliability. The inventive sintered bodies also have a good productivity and an advantageous cost efficiency.

Such superior sintered bodies are especially expected as promising structural materials which can be substituted for metallic materials heretofore used in the fields requiring a high strength level at room temperature, and also as materials for cutting tools.

### Claims

1. A silicon nitride sintered body consisting of prismatic crystal grains of Si<sub>3</sub>N<sub>4</sub> and/or sialon, equi-axed crystal grains of Si<sub>3</sub>N<sub>4</sub> and/or sialon, a grain boundary phase existing among the prismatic and equi-axed crystal grains and dispersed particles in the grain boundary phase, in which the prismatic crystal grains have an average grain size of 0.3 μm or less in minor axis and an average grain size of 5 μm or less in major axis, the equi-axed crystal grains have an average grain size of 0.5 μm or less and the dispersed particles have an average size of 0.1 μm or less, the volume of the dispersed particles being 0.05% by volume or more based on the total volume of the rest of the sintered body.
2. A silicon nitride sintered body according to Claim 1, wherein the dispersed particles have an average size of 0.03 μm or less.
3. A silicon nitride sintered body according to Claim 1, wherein the dispersed particles is at least one selected from the group consisting of compounds of Ti, Zr, Hf, V and Cr.

4. A silicon nitride sintered body according to Claim 3, wherein the dispersed particles are composed of titanium compounds and the volume of the dispersed titanium compounds is 0.05 to 4% by volume, based on the total volume of the rest of the sintered body.
5. A silicon nitride sintered body according to Claim 4, wherein the volume of the dispersed titanium compounds is 0.05 to 2% by volume, based on the total volume of the rest of the sintered body.
6. A silicon nitride sintered body according to Claim 1, wherein the silicon nitride sintered body has a strength of 160 kg/mm<sup>2</sup> or higher in terms of the three-point bending strength at room temperature according to JIS R 1601.

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FIG. I

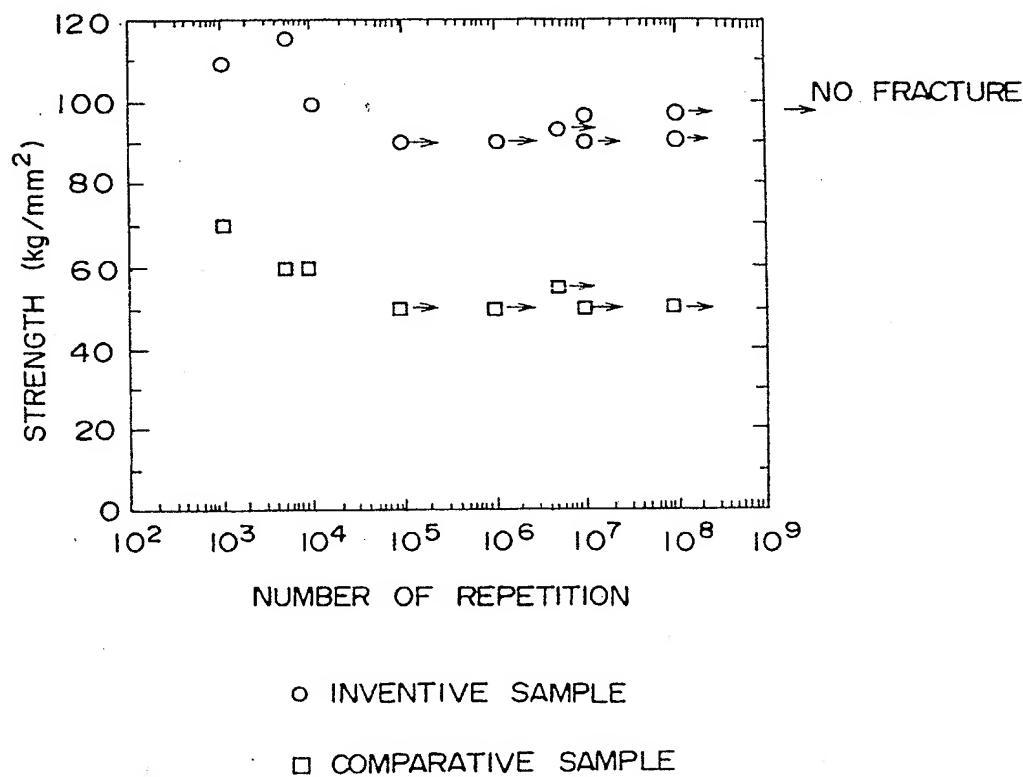


FIG. 2

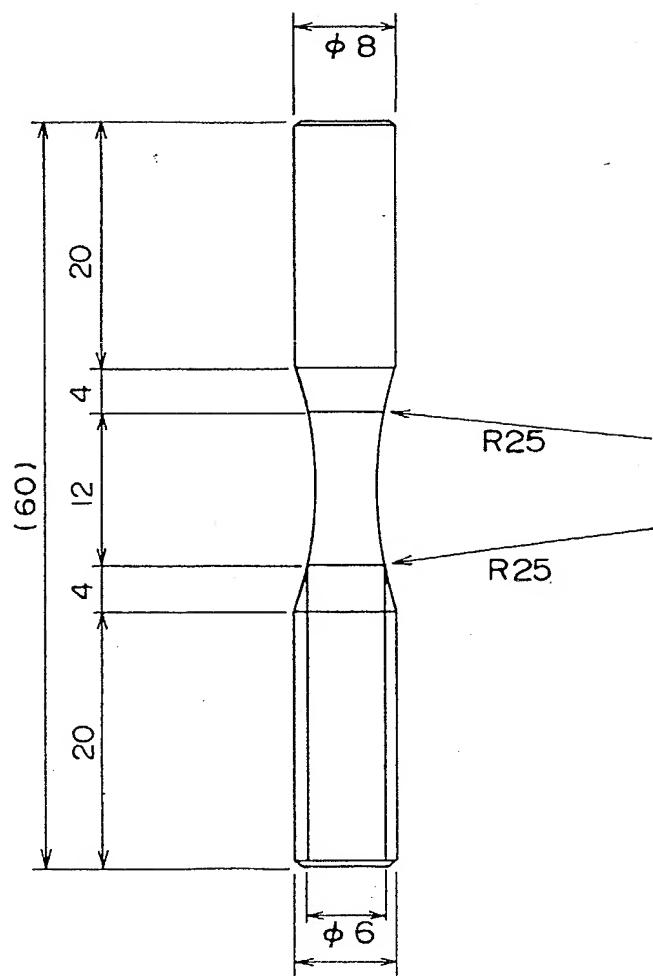
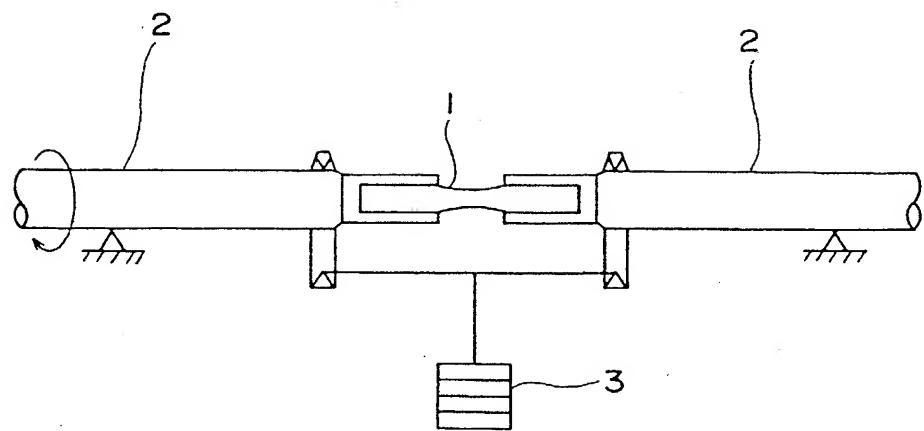


FIG. 3



# ENDEBLATT

DRUCKAUFTRAGS-ID: 604

Benutzer: mapfiste  
Drucker: gdW420\_803  
Job Beginn: 07.05.1999 12:20  
Job Ende: 07.05.1999 12:20

DEPATIS

# DRUCKAUFTRAG

605

## mapfiste

Druckauftrags-Id:

605

Benutzer:

mapfiste

Drucker:

gdW420\_803

Anforderer:

mapfiste

Gesamtkosten:

0,00 DM

Datum:

07.05.1999 12:21

DEPATIS